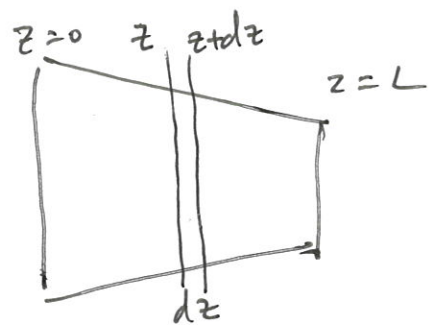


- ① For 1 dimension, $D = \frac{\Gamma a^2}{2}$
 2 dimension, $D = \frac{\Gamma a^2}{4}$
 3 dimension $D = \frac{\Gamma a^2}{6}$

As we go from 1 to 2 to 3 dimension, the random walk has more options to jump or hop in various dimension or direction. In a way, the degree of freedom of hopping increases. As a result, the net displacement will decrease. This leads to a lower diffusivity for higher dimension.

- ② (a) The system is between the two boundary conditions and where we are interested in calculating the concentration profile. In this case, the system is entire film from $z=0$ to $z=L$

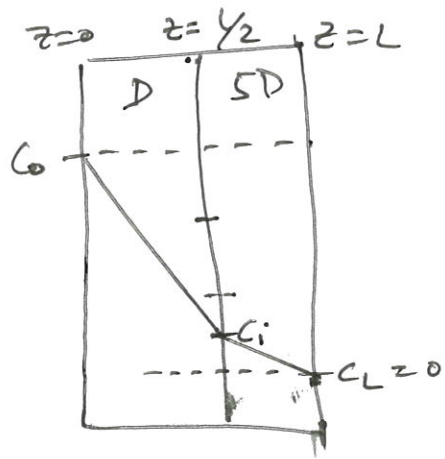


- (b) The volumetric element would be the space where the concentration is constant. In this film, it will be vertical line confined space marked in part (a)

(3) The flux at steady-state is constant.

$$\Rightarrow \left[\frac{C_0 - C_i}{(L/2)} \right] D = \left(\frac{C_i - C_L}{L/2} \right) 5D$$

Where C_i is the intermediate concentration at $z = L/2$



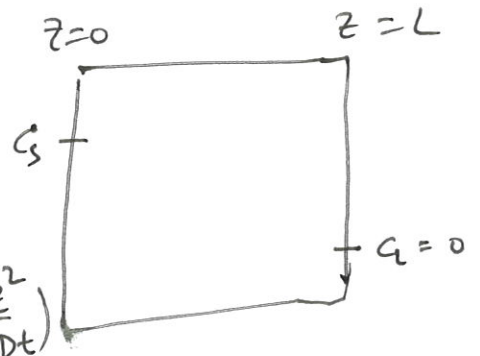
$$\Rightarrow (C_0 - C_i) = 5(C_i - C_L) = 5C_i, \quad C_L = 0$$

$$\Rightarrow C_0 = 6C_i \Rightarrow C_i = \frac{C_0}{6}$$

A rough indication is provided above.

(4) (a) Flux in the case of transient diffusion

is proportional to $\sqrt{\frac{D}{\pi t}} \exp\left(-\frac{z^2}{4Dt}\right)$



At $t=0$, flux = ∞ at $z=0$

(b) Ratio of flux at two locations at any given time =

$$\frac{\exp\left(-\frac{z_1^2}{4Dt}\right)}{\exp\left(-\frac{z_2^2}{4Dt}\right)}$$

$$\Rightarrow \frac{J_1}{J_2} = \exp\left(\frac{z_2^2 - z_1^2}{4Dt}\right) = \exp\left(\frac{z_2^2}{4Dt}\right) \text{ as } z_1 = 0$$

$$\frac{J_1}{J_2} = \exp\left(\frac{z_2^2}{4Dt}\right) \quad \text{where } z_2 = 1 \text{ cm}$$

$$D = 0.01 \text{ cm}^2/\text{s}$$

$$t = 1 \text{ s}$$

$$\Rightarrow \frac{J_1}{J_2} = \exp\left(\frac{0.01 \times 0.01}{4 \times 0.01 \times 10^{-4} \times 1}\right)$$

$$= \exp\left(\frac{100}{4}\right) = \exp(25) = 7.2 \times 10^{10}$$

This means that compared to flux at $z=0$, flux at $z=1 \text{ cm}$ is almost negligible.

- ② To calculate the total amount of gas diffusing inside the polymer, we would need to integrate the flux at $z=0$ with respect to time.

Flux at $z=0$ is $J_{z=0} = -\sqrt{\frac{D}{\pi t}} (C_0 - C_s) \exp\left(-\frac{z^2}{4Dt}\right)$

where $z=0$

Total amount of gas

$$= \int_{t=0}^{t=10\text{s}} \text{Flux} \cdot A \, dt$$

$$= A \int_0^{10\text{s}} \sqrt{\frac{D}{\pi t}} C_s \, dt = C_s A \sqrt{\frac{D}{\pi}} \int_0^{10\text{s}} \frac{dt}{\sqrt{t}}$$

⑤ Generally $n_1 = c_1 v_1$
 $n_2 = c_2 v_2$

$$n = n_1 + n_2 = c_1 v_1 + c_2 v_2$$

for gases, total concentration $c = c_1 + c_2$
 $= y_1 c + y_2 c$

$$\Rightarrow n = y_1 c v_1 + y_2 c v_2$$

$$\Rightarrow c (y_1 v_1 + y_2 v_2)$$

however, $y_1 v_1 + y_2 v_2 = v =$ average velocity of moles

$$\Rightarrow n = c v$$

⑥ Convective Flux = Average velocity \times concentration
 $= (100 \text{ km/h}) \times (\text{Water concentration})$

1 liter of water has $\frac{1000}{18}$ moles of water

$$\Rightarrow \text{Concentration of water} = 55.5 \times 10^3 \frac{\text{mol}}{\text{m}^3}$$

$$\Rightarrow \text{Flux} = \frac{100 \times 10^3}{3600} \text{ m/s} \times 55.5 \times 10^3 \frac{\text{mol}}{\text{m}^3}$$

$$\Rightarrow \text{flux} = 1.54 \times 10^6 \frac{\text{mol}}{\text{m}^2 \cdot \text{s}}$$

(7) For spherical particles which are diffusivity in water

$$D = \frac{kT}{f} \quad \text{when particle size} \gg \text{size of water molecules}$$

⇒ Ratio of Diffusion coefficient

$$\frac{D_1}{D_2} = \frac{f_2}{f_1} = \frac{r_2}{r_1} \quad \text{where } r = \text{radius of the particle}$$

$$\Rightarrow \frac{D_1}{D_2} = \frac{5}{10} = \frac{1}{2}$$

(8) (a) $D_{\text{He-Ar}} = D_{\text{Ar-He}} = 0.001 \text{ cm}^2/\text{s}$

(b) $D_2 P_2 = D_1 P_1$
 $\Rightarrow D_2 = D_1 \frac{P_1}{P_2} = 0.001 \left(\frac{1}{10} \right) = 10^{-4} \text{ cm}^2/\text{s}$

(c) $D \propto T^{3/2}$

$$\frac{D_1}{T_1^{3/2}} = \frac{D_2}{T_2^{3/2}}$$

$$\Rightarrow \frac{D_1}{D_2} = \left(\frac{T_1}{T_2} \right)^{3/2}$$

$$\begin{aligned} \Rightarrow D_2 &= D_1 \left(\frac{T_2}{T_1} \right)^{3/2} = 0.001 \left(\frac{373}{298} \right)^{1.5} \\ &= 0.001 \times 1.4 = 0.0014 \end{aligned}$$

(5)

(i) Flux is proportional to D

$$D_{vis} = \frac{d^2 P}{32\eta}, \quad D_{Knudsen} = \sqrt{\frac{8k_B T d^2}{9\eta m}}$$

$$D_{molecular} = \frac{8}{3} \sqrt{\frac{2}{m}} \left(\frac{k_B T}{\pi}\right)^{3/2} \frac{1}{P \sigma^2}$$

Note:— exact formula is not important, the aim

is to remember that

$D_{vis} \propto P$	$D_{Knudsen} \propto d$	$D_{molecular} \propto \frac{1}{P}$
$D_{vis} \propto d^2$	Independent of pressure	Independent of pore diameter

\Rightarrow we have following answer,

- a) Flux dominated by Knudsen diffusion
 viscous diffusion
- (b) " " " " Molecular diffusion
- (c) " " " " Molecular diffusion
- (d) " " " " Knudsen diffusion
- (e) " " " " viscous diffusion.
- (f) " " " "